A maintenance model with a quasi generalized Lindley distribution

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Introduction

- Lindley distribution (1958) [3, 4] was derived using the Bayes' theorem and in the last years has been in the attention of statisticians as a suitable model for lifetime data
- Lindley distribution has better properties that the exponential one (2008)[2]
- The hazard rate function of the Lindley distribution is increasing and not constant like the one of the exponential distribution
- There are many generalizations and compounding of the Lindley distribution: Pareto Poisson Lindley (2013)
 [6], beta exponentiated power Lindley (2015) [7], negative binomial Lindley (2010) [5], quasi Lindley geometric (2014) [1], beta-Lindley (2014) [2], power Lindley (2013) [3].

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Aim of paper

- Presentation of a new maintenance shock model using geometric processes
- A example of this model using Lindley type distributions
- Using the mixture of the Lindley distribution, we compare Lindley type distributions with exponential and gamma type distributions
- Simulations for the maintenance shock model

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Quasi Lindley distribution [4](2013)

Let $X \sim QGL(a, \theta)$ be a random variable quasi Lindley distributed. Then the probability density of X is

$$f(x) = \frac{\theta}{a+1}e^{-\theta x}(a+\theta x)$$

and the corresponding cumulative function

$$F(x) = 1 - \frac{a+1+\theta x}{a+1}e^{-\theta x}, \quad a > 0, \theta > 0$$
 (2)

• Mixture of gamma distributions

$$f(x) = pg(x) + (1-p)h(x)$$

where $g(x) = \theta e^{-\theta x}$, $h(x) = \theta^2 x e^{-\theta x}$ and $p = \frac{a}{a+1}$

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Hazard rate function

The hazard rate function is

$$h(x) = \frac{\theta(a + \theta x)}{a + 1 + \theta x}$$

h(x) is IFR.



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Mean and variance

The mean and the moments of order 2, 3 and 4 are

$$\mu = \frac{a+2}{\theta(a+1)}, \qquad \mu_2 = \frac{2(a+3)}{\theta^2(a+1)}, \qquad \mu_3 = \frac{6(a+4)}{\theta^3(a+1)},$$
$$\mu_4 = \frac{24(a+5)}{\theta^4(a+1)}$$

The variance of X is

$$\sigma^2 = \frac{a^2 + 4a + 2}{\theta^2 (a+1)^2}$$

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Entropy

Shannon entropy

$$H(f) = -\ln\frac{\theta^2}{a+1} + \frac{a+2}{a+1} - \frac{(a+1)(\ln a - \ln\theta) - e^a Ei(-a)}{a+1}$$

where $Ei(x) = \int_{-\infty}^{x} \frac{e^{t}}{t} dt$ is the integral exponential function Renyi entropy

$$\mathcal{J}_{R}(\gamma) = \frac{1}{1-\gamma} \left\{ 2\gamma \ln\theta + a\gamma + \ln\Gamma(\gamma+1, a\gamma) - \gamma \ln(a+1) - (\gamma+1) \ln\theta \gamma \right\}^{\text{disjuttion}}$$
$$\gamma > 0, \gamma \neq 1$$

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Generation of date

- 1. Generate $u_i \sim U(0,1)$
- 2. Generate $v_i \sim Exp(\theta)$
- 3. Generate $w_i \sim Gamma(2, \theta)$
- 4. If $u_i \leq p = \frac{a}{a+1}$ then $x_i = v_i$, otherwise $x_i = w_i$

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Transmuted quasi Lindley [4](2013)

Transmuted distributions have been introduced to model data sets in various areas

- engineering-reliability data-transmuted Weibull distribution
- finance, economics, modeling positive data- transmuted Lomax distribution
- biomedical sciences- transmuted inverse exponential distribution

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The Rank Transmutation Map (QRTM) is defined as

$$G_{R12}(u) = u + \lambda u(1-u), \quad |\lambda| \leq 1$$

Using cdf's we have the relationship

$$F_2(x) = (1+\lambda)F_1(x) - \lambda F_1(x)^2$$

and for densities

$$f_2(x) = f_1(x)[(1+\lambda) - 2\lambda F_1(x)]$$

where $f_1(x)$ and $f_2(x)$ are the corresponding probability density function associated with the cumulative density functions $F_1(x)$ and $F_2(x)$, respectively. For more details see Shaw et al. (2007)[8]. A maintenance model

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Transmuted quasi Lindley

Let
$$X \sim TQGL(a, heta, \gamma)$$
, $a, heta > 0, |\gamma| \leq 1$. The pdf is

$$f(x) = \frac{\theta}{a+1}e^{-\theta x}(a+\theta x)\left[(1-\gamma)+2\gamma\frac{a+1+\theta x}{a+1}e^{-\theta x})\right]$$

and the cdf

$$F(x) = \left[1 - \frac{a+1+\theta x}{a+1}e^{-\theta x}\right] \left[1 + \lambda \frac{a+1+\theta x}{a+1}e^{-\theta x}\right], \quad x > 0$$

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$a = 0.3, \theta = 0.2, \gamma = 0.5$ ---- $a = 0.3, \theta = 0.2, \gamma = -0.7$ $a = 1.3, \theta = 0.2, \gamma = 0.3$ $a = 2, \theta = 1, \gamma = -0.5$ 20

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The transmuted quasi Lindley has the following submodels

- $\lambda = 0$ we get the quasi Lindley distribution
- $\lambda = -1$ we get the exponentiated quasi Lindley
- a = 0 we get the transmuted gamma distribution
- $a \rightarrow \infty$ we get the transmuted exponential distribution

The mean of X is

$$\mu = \frac{(1+\gamma)(a+2)}{8(a+1)} - \frac{2\gamma}{8\theta(a+1)^2} \Big[(a+2)(8\theta - 2(a+1)) - 1 \Big]$$

The hazard rate function of X is

$$h(x) = \frac{\frac{\theta}{a+1}e^{-\theta x}(a+\theta x)\left[(1-\gamma)+2\gamma\frac{a+1+\theta x}{a+1}e^{-\theta x}\right]}{1-\left[1-\frac{a+1+\theta x}{a+1}e^{-\theta x}\right]\left[1+\gamma\frac{a+1+\theta x}{a+1}e^{-\theta x}\right]}$$

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Data generation

- 1. Generate $u_i \sim Uniform(0,1)$
- 2. Generate $v_i \sim Exp(\theta)$
- 3. Generate $w_i \sim Gamma(2, \theta)$

4. If
$$u_i otherwise $x_i = (1+\gamma)w_i - \gamma w_i^2$$$

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Figura: Data generation for $\gamma = -0.5, a = 0.3, \theta = 0.7$ and the hazard rate function

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Maintenance model

• Considering the shock model proposed by Lam. Y (2007) [5], we developed a new shock model considering two types of shocks.

• A system can be affected by multiple shock that are independent with one producing more damage than the other one, so the time of repair is greater.

• Let suppose we have a system with one component. The random external deteriorating factors reduces the functioning time of the system

Definition

[5] A sequence of nonnegative random variables $\{X_n\}_{n\geq 0}$ is said to be a geometric process (GP) if they are independent and the distribution function of X_n is given by $F(a^{n-1}x)$ for $n \geq 0$, where a > 0 is called the ratio of the GP.

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Assumptions

- We start with a newly instaled system at t=0. When the system fails it is repaired. A maintenance strategy N is adopted: the system is replaced with a new identical one after the Nth failure.
- Let X_n be the operating time of the system after the (n-1)th repair, E(X_n) > 0, (X_n)_n form a geometric process with ratio a ≥ 1.
- Let Y_n = αY_n⁽¹⁾ + (1 − α)Y_n⁽²⁾, 0 ≤ α ≤ 1 where Y_n⁽¹⁾ is the repair time of the system after the nth failure of type I, {Y_n⁽¹⁾}_{n≥0} forms a geometric process with ratio 0 < b₁ ≤ 1, E(Y₁⁽¹⁾) = μ₁ ≥ 0, and Y_n⁽²⁾ is the repair time of the system after the nth failure of type II, {Y_n⁽²⁾}_{n≥0} forms a geometric process with ratio 0 < b₂ ≤ 1, E(Y₁⁽²⁾) = μ₂ ≥ 0, μ₁ ≤ μ₂.

• Let Z be the replacement time, $E(Z) = \delta$

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The system suffers 2 kinds of shocks which occur randomly. Let N₁(t) be the number of shocks of type I by time t, (N₁(t))_t is a counting process having stationary and independent increment.

Let $N_2(t)$ be the number of shocks of type II by time t, $(N_2(t))_t$ is a counting process having stationary and independent increment.

Any shock arriving after failure gives no effect on the failed system. The succesive reductions in the system operating time are additive.

Let W_n⁽¹⁾ be the reduction in the system operating time following the nth random shock of type I, W_n⁽¹⁾ are independent identically distributed.

Let $W_n^{(2)}$ be the reduction in the system operating time following the nth random shock of type II, $W_n^{(2)}$ are independent identically distributed.

 $E(W_n^{(1)}) \leq E(W_n^{(2)})$

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- ► $\{X_n\}_n$, $(N_1(t))_{t\geq 0}$, $(N_2(t))_{t\geq 0}$, $(W_n^{(1)})_n$ and $(W_n^{(2)})_n$ are independent
- Let r be the reward rate of the system and c the average cost of repair. The cost of replacement has two parts: the basic costs R and a part that is proportional with the time of replacement Z, with rate c_p representing the cost of labor, energy, etc.
- The number of shocks in $(t_{n-1}, t_{n-1} + t]$ is

$$N(t_{n-1}, t_{n-1} + t] = N(t_{n-1} + t) - N(t_{n-1})$$

where $N(t_{n-1})$ is the number of shocks until t_{n-1} time and $N(t_{n-1} + t)$ the number of shocks until $t_{n-1} + t$ time.

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$$N(t_{n-1}) = N_1(t_{n-1}) + N_2(t_{n-1})$$

$$N(t_{n-1}+t) = N_1(t_{n-1}+t) + N_2(t_{n-1}+t)$$

where $N_1(t_{n-1})$ and $N_2(t_{n-1})$ are the number of shocks of type I, type II, respectively until t_{n-1} and $N_1(t_{n-1} + t)$ and $N_2(t_{n-1} + t)$ are the number of shocks of type I, type II, respectively until $t_{n-1} + t$.

The total functioning reduced time in (t_{n-1}, t_{n-1} + t] is

$$TR_{(t_{n-1},t_{n-1}+t]} = \sum_{i=N_1(t_{n-1})+1}^{N_1(t_{n-1}+t)} W_i^{(1)} + \sum_{i=N_2(t_{n-1})+1}^{N_2(t_{n-1}+t)} W_i^{(2)}$$
$$= \sum_{i=1}^{N_1(t_{n-1},t_{n-1}+t)} W_i^{(1)} + \sum_{i=1}^{N_2(t_{n-1},t_{n-1}+t)} W_i^{(2)}$$

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The residual time at $t_{n-1} + t$ time is

$$S_n(t) = X_n - t - TR_{(t_{n-1}, t_{n-1}+t]}$$

If $S_n(t) < 0$, then the system fails. The real functioning time of the system after the (n-1)th repair is given by

$$X_n' = \inf_{t\geq 0} \{t|S_n(t)\leq 0\}$$

Lemma

$$P(X_n = t - TR_{(t_{n-1}, t_{n-1} + t]} > 0, \forall t \in [0, t'])$$

= $P(X_n - t' - TR_{(t_n - 1)}, t_{n-1} + t'] > 0)$

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For the real operating time of the system we have

$$P(X'_{n} > t' | N_{1}(t_{n-1}, t_{n-1} + t') = k_{1}, N_{2}(t_{n-1}, t_{n-1} + t') = k_{2})$$

= $1 - \int_{0}^{\infty} F_{n}(t' + x) dH_{k_{1},k_{2}}(x) dx$ (3)

where $F_n(x) = F(a^{n-1}x)$ and $H_{k_1,k_2}(x)dx$ are the cumulative distribution function of X_n and $\sum_{i=1}^{k_1} W_i^{(1)} + \sum_{i=1}^{k_2} W_i^{(2)}$, respectively.

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The real operating time of the system is

$$P(X'_{n} \leq x) = \sum_{k_{1}=0}^{\infty} \sum_{k_{2}=0}^{\infty} \int_{0}^{\infty} F_{n}(x+\omega) dH_{k_{1},k_{2}}(\omega) \times P(N_{1}(x) = k_{1}) P(N_{2}(x) = k_{2})$$
(4)

We say a cycle is complet when a replacement is complet. So, consecutive cycles together with the corresponding costs form a renewal reward process. [5]. A maintenance model

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Using the replacement strategy N: the system is replaced with a new identical one after the Nth failure, we obtain the following average cost:

$$C(N) = \frac{E[c\sum_{n=1}^{N-1} Y_n - r\sum_{n=1}^{N} X'_n + R + c_p Z]}{E[\sum_{n=1}^{N-1} X'_n + \sum_{n=1}^{N-1} Y_n + Z]}$$

$$= \frac{c\alpha\mu_1 \sum_{n=1}^{N-1} \frac{1}{b_1^{n-1}} + c(1-\alpha)\mu_2 \sum_{n=1}^{N-1} \frac{1}{b_2^{n-1}} - r\sum_{n=1}^{N} \lambda'_n + R}{\sum_{n=1}^{N-1} \frac{1}{b_1^{n-1}} + c(1-\alpha)\mu_2 \sum_{n=1}^{N-1} \frac{1}{b_2^{n-1}} - r\sum_{n=1}^{N} \lambda'_n + R}{\sum_{n=1}^{N} \lambda'_n + R} + \frac{Color B}{Color B}$$

$$= P(N) - r$$

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where
$$\lambda'_n = E(X'_n)$$
 and

$$P(N) = \frac{(c+r)\left[\mu_1 \alpha \sum_{n=1}^{N-1} \frac{1}{b_1^{n-1}} + \mu_2(1-\alpha) \sum_{n=1}^{N-1} \frac{1}{b_2^{n-1}}\right] + R + c_p \delta^{\alpha + r} \delta_{\text{Replacement}}}{\sum_{n=1}^{N} \lambda'_n + \alpha \mu_1 \sum_{n=1}^{N-1} \frac{1}{b_1^{n-1}} + (1-\alpha)\mu_2 \sum_{n=1}^{N-1} \frac{1}{b_2^{n-1}} + \delta_{\text{Maintenance model}}}^{\text{Results}}$$
Conclusions

Let h(N) = $\overline{(R+c_{p}\delta+r\delta)\Big[(b_{1}b_{2})^{N-1}\lambda_{N+1}^{\prime}+\alpha\mu_{1}b_{2}^{N-1}+\mu_{2}(1-\alpha)b_{1}^{N_{m}}}^{N_{m}}$ $\times \left\{ (c+r) \Big[(b_2^{N-1} \mu_1 \alpha + \mu_2 (1-\alpha) b_1^{N-1}) \sum_{i=1}^N \lambda'_n \right]$ $-\lambda'_{N+1}(b_2^{N-1}\mu_1\alpha\sum^{N-1}b_1^n+b_1^{N-1}\mu_2(1-\alpha)\sum^{N-1}b_2^n)$ and the transmuted $+ \delta(\mu_1 \alpha b_2^{N-1} + \mu_2(1-\alpha)b_1^{N-1}) \bigg] \bigg\}$

We have the following results

Lemma

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\lambda'_n is a nonincreasing function in n
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Lemma

h(N) is a nondecreasing function in N

Theorem

The optim replacement strategy N^* is determined so that

 $N^* = \min\{N | h(N) \ge 1\}$

 N^* is unique if and only if $h(N^*) > 1$.

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Conclusions

• Considering the extended model proposed we consider two cases and for each of it simulation application. We consider the reduction times in the system operating time to be exponential distributed, $W_n^{(1)} \sim Exp(\lambda_1)$ and $W_n^{(2)} \sim Exp(\lambda_2)$, $\lambda_1 \leq \lambda_2$ and 2 cases

► Case 1
$$(X_n)_n \sim QGL(a_1, \theta_1)$$
 and
 $(Y_n^{(1)})_n \sim QGL(a_2, \theta_2), (Y_n^{(2)})_n \sim QGL(a_3, \theta_3)$

► Case 2
$$(X_n)_n \sim TQGL(a_1, \theta_1, \gamma_1)$$
 and
 $(Y_n^{(1)})_n \sim TQGL(a_2, \theta_2, \gamma_2), (Y_n^{(2)})_n \sim TQGL(a_3, \theta_3, \gamma_3)$

• We consider also that $(N_1(t))_t$ and $(N_2(t))_t$ are Poisson processes of intensity λ_{N_1} and λ_{N_2} .

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Theorem

[5](2014) Let $X_i \sim \text{Gamma}(\alpha_i, \beta_i)$, $\alpha_i, \beta_i > 0$, $i = \overline{1, n}$, independent and $S = X_1 + \cdots + X_n$. Let

 $X_m \sim Gamma(\alpha_m, \beta_m)$ denote the approximating gamma distribution of S associated with the moment matching method. We have

$$E(X_m) = \alpha_m \beta_m, \quad E(S) = \sum_{i=1}^n \alpha_i \beta_i$$

$$Var(X_m) = \alpha_m \beta_m^2, \quad Var(S) = \sum_{i=1}^n \alpha_i \beta_i^2$$

n

where
$$\alpha_m = \frac{\mu^2}{\sum_{i=1}^n \alpha_i \beta_i^2}$$
, $\beta_m = \frac{\sum_{i=1}^n \alpha_i \beta_i^2}{\mu}$ and $\mu = \sum_{i=1}^n \alpha_i \beta_i$

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The distribution of
$$\sum_{i=1}^{k_1} W_i^{(1)} + \sum_{i=1}^{k_2} W_i^{(2)}$$
 is given by the

following theorem

Theorem
Let
$$S = \sum_{i=1}^{k_1} W_i^{(1)} + \sum_{i=1}^{k_2} W_i^{(2)}$$
. Then

$$S \sim Gamma(\alpha_m, \beta_m)$$

, where

$$\alpha_m = \frac{(k_1\lambda_1 + k_2\lambda_2)^2}{k_1\lambda_1^2 + k_2\lambda_2^2}, \quad \beta_m = \frac{k_1\lambda_1^2 + k_2\lambda_2^2}{k_1\lambda_1 + k_2\lambda_2}$$

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Case 1

The probability function of the real functioning time of the system after the (n-1)th repair is

$$P(X'_{n} \leq x) = \sum_{k_{1}=0}^{\infty} \sum_{k_{2}=0}^{\infty} \left\{ 1 - \frac{e^{-\theta_{1} \times a^{n-1}}}{(a_{1}+1)\beta_{m}^{\alpha_{m}} \Gamma(\alpha_{m})} I \right\}$$
$$\times \frac{e^{-\lambda_{N_{1}}} x (\lambda_{N_{1}} x)^{k_{1}}}{k_{1}!} \frac{e^{-\lambda_{N_{2}}} x (\lambda_{N_{2}} x)^{k_{2}}}{k_{2}!}$$

where $I = \theta_1 a^{n-1} z^{\alpha_m+1} \Gamma(\alpha_m) \Psi(\alpha_m, \alpha_m+2, \lambda_{\Psi} z)$, $\lambda_{\Psi} = \theta_1 a^{n-1} + \frac{1}{\beta_m}, z = \frac{a_1+1+\theta_1 \times a^{n-1}}{\theta_1 a^{n-1}}; \Gamma(s) = \int_0^\infty x^{s-1} e^{-x} dx$ is the gamma function and $\Psi(\cdot, \cdot, \cdot)$ Kummer function, $\Psi(a, b, u) = \frac{1}{\Gamma(a)} \int_0^\infty t^{a-1} (1+t)^{b-a-1} e^{-ut} dt, \quad Re(a), Re(u) > 0, b \in \mathbb{C}$

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• For
$$\lambda_1 = \lambda_2 = 1$$
, $\lambda_{N_1} = 3$, $\lambda_{N_2} = 0.5$, $\delta = 4$, $r = 5$, $c = 5$, $R = 10$, $c_p = 5$, $\alpha = 0.4$, $b_1 = 0.87$, $b_2 = 0.7$, $a = 2$ and
• $a_1 = 0.02$, $\theta_1 = 2$, $a_2 = 0.03$, $\theta_2 = 3$, $a_3 = 0.05$, $\theta_3 = 2$

we have

Tabela: Case 1.1

Ν	h(N)	C(N)	N	h(N)	C(N)
20	0.7854168	4.753316	27	1.055361	4.971424
21	0.8246262	4.816599	28	1.093465	4.97922
22	0.8638435	4.864317	29	1.131432	4.984915
23	0.9023237	4.900046	30	1.169358	4.989065
24	0.9406939	4.926618			
25	0.9790204	4.946283			
26	1.017254	4.960777			

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• $a_1 = 1.7, \theta_1 = 4, a_2 = 3, \theta_2 = 7, a_3 = 4, \theta_3 = 2$ we have

Tabela: Case 1.2

Ν	h(N)	C(N)	N	h(N)	C(N)
20	0.7636672	4.613763	27	1.02722	4.954912
21	0.8018419	4.712099	28	1.063932	4.96722
22	0.8397631	4.786613	29	1.100854	4.97621
23	0.8773941	4.842579			
24	0.9153349	4.884313			
25	0.9527026	4.915274			
26	0.9897275	4.938122			

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• $a_1 = 100, \theta_1 = 4, a_2 = 3000, \theta_2 = 7, a_3 = 4000, \theta_3 = 2$ we have



Ν	h(N)	C(N)	Ν	h(N)	C(N)
20	0.7593386	4.543052	27	1.021854	4.946206
21	0.7974994	4.658628	28	1.059124	4.960862
22	0.8353168	4.746551	29	1.096204	4.97158
23	0.8729748	4.812782			
24	0.9103821	4.862286			
25	0.947708	4.899051			
26	0.9848449	4.926218			

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Figura: Case 1.1 and Case 1.2

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Figura: Case 1.3

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Case 2

The probability function of the real functioning time of the system after the (n-1)th repair is

$$P(X_{n}^{'} \leq x) = \sum_{k_{1}=0}^{\infty} \sum_{k_{2}=0}^{\infty} \left\{ 1 + \frac{e^{-\theta_{1}xa^{n-1}}}{(a_{1}+1)\beta_{m}^{\alpha_{m}}\Gamma(\alpha_{m})} I(\gamma-1) - \gamma J \right\}$$
$$\times \frac{e^{-\lambda_{N_{1}}}x(\lambda_{N_{1}}x)^{k_{1}}}{k_{1}!} \frac{e^{-\lambda_{N_{2}}}x(\lambda_{N_{2}}x)^{k_{2}}}{k_{2}!}$$

where
$$I = \theta_1 a^{n-1} z^{\alpha_m+1} \Gamma(\alpha_m) \Psi(\alpha_m, \alpha_m + 2, \lambda_{\Psi} z)$$
,
 $\lambda_{\Psi} = \theta_1 a^{n-1} + \frac{1}{\beta_m}$, $z = \frac{a_1 + 1 + \theta_1 x a^{n-1}}{\theta_1 a^{n-1}}$ and
 $J = \frac{e^{-2\theta_1 x a^{n-1}} \theta_1^2 a^{2(n-1)}}{(a_1+1)^2 \beta_m^{\alpha_m} \Gamma(\alpha_m)} z^{\alpha_m+2} \Gamma(\alpha_m) \Psi(\alpha_m, \alpha_m + 3, \lambda_{\Psi}^* z)$,
 $\lambda_{\Psi}^* = 2\theta_1 a^{n-1} + \frac{1}{\beta_m}$

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• For
$$\lambda_1 = \lambda_2 = 1$$
, $\lambda_{N_1} = 3$, $\lambda_{N_2} = 0.5$, $\delta = 4$, $r = 5$, $c = 5$, $R = 6$, $c_p = 3$, $\alpha = 0.7$, $b_1 = 0.3$, $b_2 = 0.8$, $a = 2$ and
• $a_1 = 0.5$, $\theta_1 = 8$, $\gamma_1 = -0.5$, $a_2 = 0.7$, $\theta_2 = 4$, $\gamma_2 = -0.6$, $a_3 = 0.4$, $\theta_3 = 10$, $\gamma_3 = -0.9$ we have

Tabela: Case 1.3

Ν	h(N)	C(N)	
10	0.7887837	4.990034	
11	0.851982	4.996723	
12	0.9133332	4.998933	
13	0.974314	4.999655	
14	1.033471	4.999889	
15	1.09242	4.999965	
16	1.152533	4.999989	

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Figura: Case 2

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Conclusions

- There isn't a huge difference between the quasi Lindley distribution and the exponential and gamma distribution in terms of the maintenance model
- Using the new model we can develop replacements strategies for systems that are subjected to multiple shocks that come at the same moment or not

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